BRITISH OCCUPATIONAL HYGIENE SOCIETY

HYDROCARBON DISTILLATE VAPOUR COMPOSITION

- Prediction by Microcomputer

Technical Guide Series, No. 2

| | TECHNICAL GUIDE SERIES |
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| No. 1 No. 2 | Statistical Analysis of Monitoring Data by Microcomputer. August 1983 Hydrocarbon Distillate Vapour Composition – Prediction by Microcomputer. October 1983 |
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HYDROCARBON DISTILLATE VAPOUR COMPOSITION PREDICTION BY MICROCOMPUTER

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A Basic programme for calculating the composition and concentration of vapours from the surface of bulk hydrocarbon distillate liquids.

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HYDROCARBON DISTILLATE VAPOUR COMPOSITION PREDICTION BY MICROCOMPUTER

by D.T. Coker

This is the second paper in the series from the BOHS Technology Committee giving applications and programmes for microcomputers which may be of use to the occupational hygienist. The Committee would welcome any programmes from hygienists to include in this series, covering any aspect of occupational hygiene.

The application and programme given here is for predicting the composition and concentration of vapours arising from evaporation from the surface of bulk hydrocarbon distillate liquids. The vapour composition is typically very different to the liquid, but can be predicted using Raoults Law for perfect gas behaviour and equilibrium conditions.

This prediction gives a reasonable estimate of the vapour composition, but if better accuracy is required then more complex calculations involving activity coefficients must be used - such as in the American Petroleum Institute's VAPRAT programme.

Hydrocarbons behave as near perfect gases and conditions close to equilibrium occur when evaporation is from a bulk liquid into a still, enclosed headspace, at a steady temperature and pressure. However a different composition - closer to the liquid composition - will occur when evaporation is from a thin film such as a wet surface. The range of vapour compositions possible therefore is limited between the liquid composition and the predicted composition.

Raoults Law states that:

The mole fractions of mixture components can be calculated from their weight percent in the mixture and their molecular weights.

Calculating Vapour Pressure

SVP's for hydrocarbons can be read from the graph (Figure 1). However for computing it is more convenient to use a mathematical expression⁽¹⁾. The following expression gives the SVP's for hydrocarbons from C No.4 and above with a good degree of accuracy.

$$P_{C} = 10 \frac{\left(\frac{2.881 - \phi \Delta t}{273 + t - 0.15 \Delta t}\right)}{10}$$

where t = temperature for the calculation in °C

At = difference between t and the boiling point of component C

 $P_c = SVP \text{ of component } C \text{ (in mmHg)}$

 ϕ = Entropy of Vapourisation
(B.Pt $^{\circ}$ C x 0.00205 + 4.54 for hydrocarbons)----3

This does not give an accurate value for C 1 to 3 hydrocarbons and a separate expression is required for each. (These are given in the programme).

Component Crouping

It is obviously rather impractical to calculate the composition of all the many hundreds of possible components in a distillate, but a convenient condensation can be made by grouping as follows:

- saturates + olefines by carbon number
- aromatics by carbon number

As the SVP's are very low above carbon number 13 this is used as the upper limit, any components of higher carbon number can be included with C. No. 13.

The composition of the vapour is often used for calculating Exposure Limits and so certain key substances with individual exposure limits are included separately. These are:

cyclohexane
nllexane
trimethylbenzenes
isopropylbenzene
naphthalene
benzene (as C₆ aromatic)

This composition can be obtained by a standard GC analysis.

The boiling point of each carbon number group of saturates is taken as the n-paraffin and in the second group as a mean figure for the most common alkylbenzenes. These boiling points and their calculated φ values and molecular weights are given in Table 1.

| + | Saturates Olefines | BP ^o C | ¢ | M.W. | Aromatics | BP ^O C | ф | M.W. |
|---|-----------------------|-------------------|------|------|--------------|-------------------|------|------|
| С | No. 1 | -164 | 4.20 | 16 | | | | |
| | 2 | - 88 | 4.36 | 30 | C No. 6 | 80 | 4.70 | 78 |
| | 3 | - 42 | 4.45 | 44 | 7 | 111 | 4.77 | 92 |
| | 4 | - 1 | 4.54 | 58 | 8 | 140 | 4.83 | 106 |
| | 5 | 36 | 4.61 | 72 | 9 | 165 | 4.88 | 120 |
| | 6 | 69 | 4.68 | 86 | 10 | 185 | 4.92 | 134 |
| | 7 | 98 | 4.74 | 100 | 11 | 205 | 4.96 | 148 |
| | 8 | 126 | 4.80 | 114 | 12 | 226 | 5.01 | 162 |
| | 9 | 151 | 4.85 | 128 | 13 | 245 | 5.05 | 176 |
| | 10 | 174 | 4.90 | 142 | Trimethyl Bz | 170 | 4.89 | 120 |
| | 11 | 196 | 4.94 | 156 | Isopropyl Bz | 152 | 4.85 | 120 |
| | 12 | 216 | 4.99 | 170 | Naphthalene | 218 | 4.99 | 128 |
| | 13 | 236 | 5.03 | 184 | Cyclohexane | 81 | 4.71 | 84 |
| | | İ | | | n-Hexane | 69 | 4.68 | 86 |
| | | 1 | - | ! | | 1 | 1 | I |

An alternative to using the carbon number analysis above is to estimate total carbon number distribution from the distillation curve, using the above boiling points or a GC distillation and an aromatics GC analysis. Aromatics are then subtracted from the relevant carbon number.

Calculation Procedure

The vapour composition can now be calculated from liquid compositional analysis in a series of steps as shown in the example in the following tabulation.

| | | | A | В | С | |
|------------------|---------|---------------------------------|--------------------------------|---------------------------------------|--|--------------------------------|
| Croup | WE X | Mole fraction (wt % / MW) | Normalised Mole fraction | Calculated SVP @ 20°C (umoHg) | Partial Pressure A X B (mmHg) | Vol Z Composition C/7.60 |
| c ₄ | 10 | .172 | .144 | 1596 | 230 | 30.3 |
| c ₅ | 20 | .278 | .232 | 424 | 98.4 | 12.9 |
| c ₆ | 20 | .233 | .194 | 120 | 23.3 | 3.1 |
| c ₇ | 15 | .150 | .125 | 36.8 | 4.60 | 0.61 |
| c ₈ | 5 | .044 | .037 | 11.1 | .41 | 0.05 |
| C ₆ A | 5 | .064 | .053 | 77.3 | 4.10 | 0.54 |
| C7A | 15 | .163 | .136 | 21.2 | 2.88 | 0.38 |
| C8A | 10 | .094 | .078 | 5.9 | .46 | 0.06 |
| | Σ = 100 | Σ =1.198 | Σ=1 | | Σ364.2 | |
| | | | | Total | vapour press | ure 47.9 |

- Step 1 Divide the weight percent of each group by its molecular weight
- Step 2 Normalise these to give a sum of 1This is the molar fraction of the group (A)

- Step 3 Calculate the Saturated Vapour Pressures for each group at the required temperature from equations (2) and (3) or from Figure 1.

 The units will be in mmHg (B)
- Step 4 Calculate the partial pressures of each group by multiplying the molar fractions by the SVP's (A X B = C) units will be mmHg
- Step 5 Sum the partial pressures for each group to give the Total Vapour Pressure in mmHg
- Step 6 Calculate the volume percent composition of the vapour by dividing by 7.60, or multiply by 100

Total Vapour Pressure

to give composition normalised to 100% (i.e. excluding air).

Computer Programme

A Computer programme is given in Appendix 1 written in Microsoft Basic for a Commodore PET 2001. This inputs liquid composition for the component groups and calculates vapour composition at the required temperature. It also calculates the average molecular weight for each composition and the total % hydrocarbon vapour. The calculations can then be repeated for any temperature.

Some alterations may be necessary for other variants of Basic such as "LET" and "RESTORE" commands, and these will need to be checked by the user to ensure the calculations are properly executed. The tabulation of results starting line 800 may also need to be TABbed in some computers.

The input composition must add up to 99 to 101%. The values for the 5 individual substances must also be included in their respective carbon number groups, i.e. n-Hexane and Cyclohexane in Sats. C. No. 6; Trimethylbenzenes and isopropylbenzene in Aromatics C. No. 9; Naphthalene in Aromatics C. No. 10.

COMPOSITION OF TEST SET

| COMPONENT | LIQUID WT Z | VAPOUR @ 13°C | MEASURED VAPOUR @ 13°C VOL Z | | |
|--------------------------|----------------|---------------|------------------------------|--|--|
| | | | | | |
| SATS. C No 1 | o | 0 | 0 | | |
| SATS. C No 2 | 0 | 0 | 0 | | |
| SATS. C No 3 | .3 | 12,24 | 11.2 | | |
| SATS. C No 4 | 7.6 | 56.33 | 53.5 | | |
| SATS. C No 5 | 14.8 | 22.4 | 25.0 | | |
| SATS. C No 6 | 18.4 | 6.29 | 7.5 | | |
| SATS. 'C No 7 | 7.8 | .68 | 1.2 | | |
| SATS. C No 8 | 4.7 | .1 | 0.2 | | |
| SATS. C No 9 | 1.7 | .01 | .02 | | |
| SATS. C No 10 | 2.7 | 0 | 0 | | |
| SATS. C No 11 | . 89 | 0 | 0 | | |
| SATS. C No 12 | 0 | 0 | 0 | | |
| SATS. C No 13 | 0 | 0 | 0 | | |
| AROMS C No 6 | 4.5 | 1.08 | 0.9 | | |
| AROMS C No 7 | 12.7 | .68 | .49 | | |
| AROMS C No 8 | 14.1 | .17 | .1 | | |
| AROMS C No 9 | 5.9 | .02 | .01 | | |
| AROMS C No 10 | 3.9 | 0 | 0 | | |
| AROMS C No 11 | 0 | 0 | 0 | | |
| AROMS C No 12 | 0 | 0 | 0 | | |
| AROMS C No 13 | 0 | 0 | 0 | | |
| CYCLOHEXANE | 0 | o | 0 | | |
| N-HEXANE | 3.5 | 1.2 | 1.5 | | |
| TRIMETHYLBENZENES | , 3.9 | .01 | 0 | | |
| ISOPROPYLBENZENE | 0 | 0 | 0 | | |
| NAPHTHALENE | 0 | 0 | 0 | | |
| BENZENE | 4.5 | 1.08 | 0.9 | | |
| AVE. MOL WTS: | 94 | 62.1 | | | |
| TOTAL %VOL H/C IN VAPOUR | 34.461 | | | | |

PETVAP PROGRAMME SUMMARY

| Line Nos. | Function | | | | |
|-------------|---|--|--|--|--|
| 10 - 40 | Heading | | | | |
| 110 - 400 | Inputs liquid composition, calculates mol fractions, sums input percentages and mol fractions | | | | |
| 430 - 480 | Checks liquid composition adds up to 99 to 101% | | | | |
| 520 \$ 700 | Boiling points of components (Sats and Aromatics) | | | | |
| 530 - 776 | Calculates partial pressure of the following components and sums total partial pressure | | | | |
| 590 | Methane | | | | |
| 610 | c_2 | | | | |
| 630 | c_3 | | | | |
| 660 | Saturates C ₄ to C ₁₃ | | | | |
| 740 | Aromatics C ₆ to C ₁₃ | | | | |
| 775 | The 5 individual hydrocarbons | | | | |
| 790 | Left free for line printer output commands | | | | |
| 800 - 820 | Output table headings | | | | |
| 830 - 950 | Prints output table of: Component: * wt in liquid: % vol in vapour (normalised to 100%) | | | | |
| 970 - 1110 | Calculates and prints average molecular weight of liquid and vapour, and total vapour concentration | | | | |
| 1130 | Is left free for line printer termination commands | | | | |
| 1140 - 1200 | Allows the procedure to be repeated for another temperature | | | | |

PROGRAMME LISTING

```
10 PRINT"PETVAP - THIS PROGRAMME PREDICTS VAPOUR"
20 PRINT"COMPOSITION FROM LIQUID COMPOSITION FOR"
30 PRINT"FETROLEUM DISTILLATES.IT ALSO CALCULATES"
40 PRINT"OEL'S, AVERAGE MOL WTS AND %VAPOUR IN AIR"
50 PRINT
60 PRINT"ENTER NAME OF PRODUCT"
70 INPUT A≸
80 PRINT
90 X=0:Z=0:G=0:E1=0:E2=0:N=6
100 DIM A(13),B(13),C(13),D(13),K(N),J(N),H(13),L(13),R(N)
110 PRINT"ENTER LIQUID COMPOSITION IN WTX"
120 FOR I=1T013
130 PRINT"SATS. C NO"; I;
140 INPUT A(I)
150 H(I)=A(I)/(2+I*14)
160 X=X+A(I)
170 Z=Z+H(I)
180 NEXT I
270 FOR I=6T013
280 PRINT"AROMATICS C NO";I;
290 INPUT C(I)
300 L(I)=C(I)/(14*I-6)
310 X=X+C(I)
320 Z≃Z+L(I)
330 NEXT I
340 DATA 84,"CYCLOHEXANE",86,"N-HEXANE",120,"TRIMETHYLBENZENES"
345 DATA120, "ISOPROPYLBENZENE", 128, "NAPHTHALENES"
350 FOR I=1TO(N-1)
360 READ P,Q$
370 PRINT Q$;
380 INPUT J(I)
390 R(I)=J(I)/P
400 NEXT I
430 IF XC99 THEN460
440 IF X>101 THEN460
450 GOTO490
460 PRINT"TOTAL IS";X;".IT MUST BE BETWEEN 99 AND 101"
470 PRINT"TRY AGAIN"
475 RESTORE
477 X=0:Z=0
480 GOTO 110
490 PRINT
500 PRINT"ENTER TEMPERATURE IN DEG. C";
510 INPUT J
520 DATA -1,36,69,98,126,151,174,196,216,236
530 FOR I=1T013
 540 B(I)=H(I)/Z
 550 IF I>3 THEN650
 560 IF I=1 THEN590
 570 IF I=2 THEN610
580 IF I=3 THEN630
 590 B(I)=10†(6.89604-(449.746/(J+273)))*B(I)/7.6
 600 GOTO 670
 610 B(I)=10†(7.36795-(835.928/(J+273)))*B(I)/7.6
 620 GOTO 670
 630 B(I)=10↑(7.18659-(990.853/(J+273)))*B(I)/7.6
 640 GOTO 670
 650 READ Q
```

```
660 B(I)=101(2.8808-(((Q*.00205+4.54)*(Q-J))/((273+J)-.15*(Q-J))))*B(I)/7.6
670 G=G+B(I)
690 NEXT I
700 DATA 80,111,140,165,185,199,226,245
710 FOR I=6T013
720 D(I)=L(I)/Z
730 READ Q
740 D(I)=101(2.8808-(((Q*.00205+4.54)*(Q-J))/((273+J)-.15*(Q-J))))*D(I)/7.6
750 G=G+D(I)
770 NEXT I
771 DATA 81,69,170,152,218
772 FOR I=1TO(N-1)
773 K(I)=R(I)/Z
774 READ Q
775 K(I)=101(2.8808-(((Q*.00205+4.54)*(Q-J))/((273+J)-.15*(Q-J))))*K(I)/7.6
776 NEXT I
780 PRINT
800 PRINT,,"COMPOSITION OF ";A$
810 PRINT,,"LIQUID","VAPOUR AT";J;"DEG C"
820 PRINT"COMPONENT","WTX","VOLX"
830 PRINT"-
840 FOR I=1T013
850 PRINT"SATS. C NO"; I,A(I), INT((B(I)*100/G)*100+.5)/100
860 NEXT I
890 FOR I=6T013
900 FRINT"AROMS. C NO";I,C(I),INT((D(I)*100/G)*100+.5)/100
910 NEXT I
920 DATA"CYCLOHEXANE", "N—HEXANE", "TRIMETHYLBENZENES", "ISOPROPYLBENZENE"
925 DATA"NAPHTHALENE", "BENZENE"
927 K(6)=D(6):J(6)=C(6)
930 FOR I=1TON
933 READ Q$
935 FRINT Q$,J(I),INT((K(I)*100/G)*100+.5)/100
940 NEXT
950 PRINT"
960 PRINT
970 FOR I=1T013
980 E1=E1+(A(I)/100)*(2+I*14)
990 E2=E2+(B(I)/G)*(2+I*14)
1000 NEXT I
1030 FOR I=6T013
1040 E1=E1+(C(I)/100)*(14*I-6)
1050 E2=E2+(D(I)/G)*(14*I-6)
1060 NEXT
1090 PRINT"AVE. MOL WTS:",INT(E1*10+.5)/10,INT(E2*10+.5)/10
1100 PRINT
1110 PRINT"TOTAL WVOL H/C IN VAFOUR"; INT(G*1000+.5)/1000
1120 PRINT
1140 PRINT"ENTER NEXT TEMPERATURE"
1150 RESTORE
1160 G=0:E1=0:E2=0
1170 FOR I=1TON-1
1180 READ 0.P$
1190 NEXTI
1200 GOTO 510
1210 END
```

